

# **EE105**

## **Microelectronic Devices and Circuits**

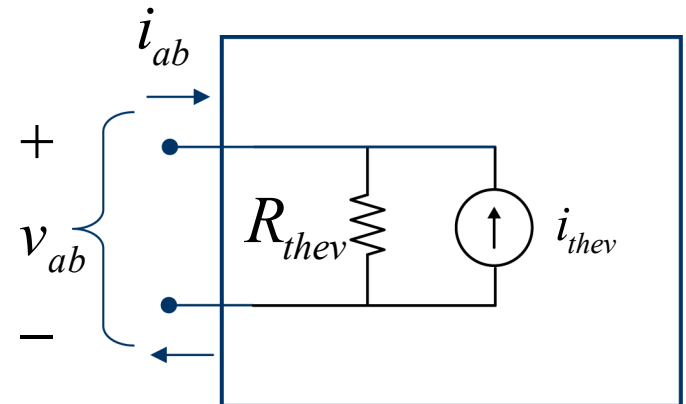
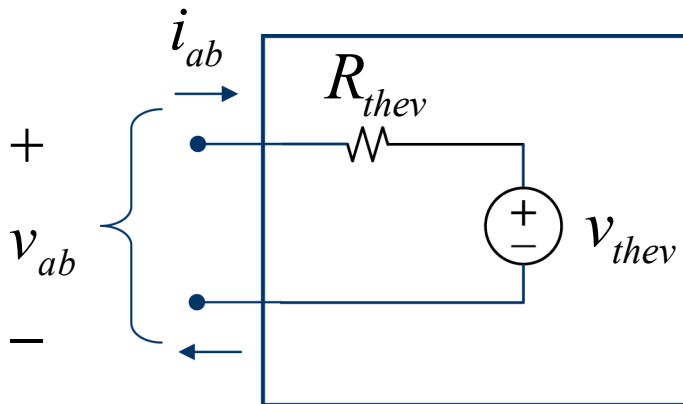
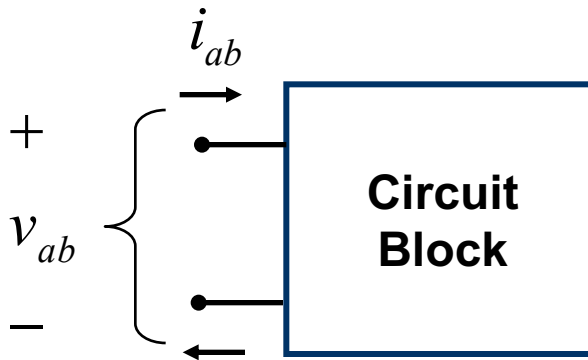
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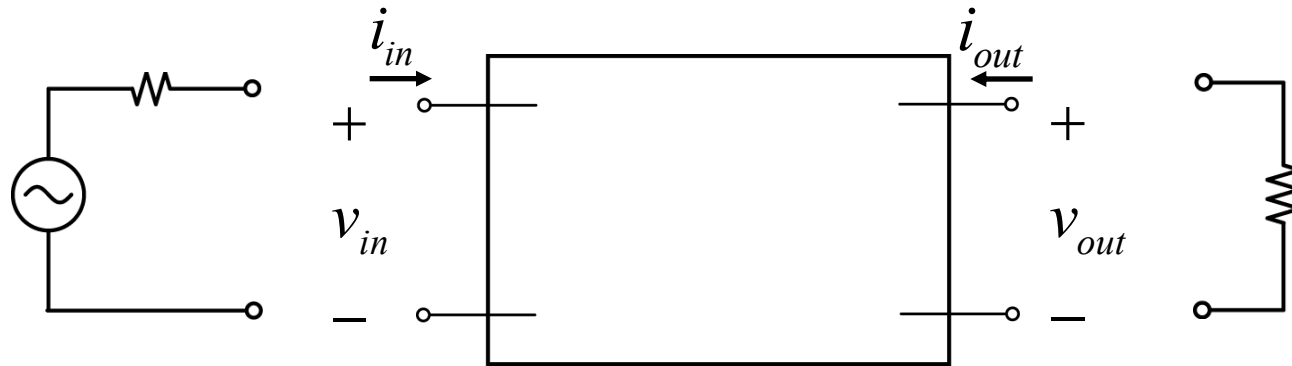
**511 Sutardja Dai Hall (SDH)**

# One-Port Models (EECS 16A)

- A terminal pair across which a voltage and associated current are defined

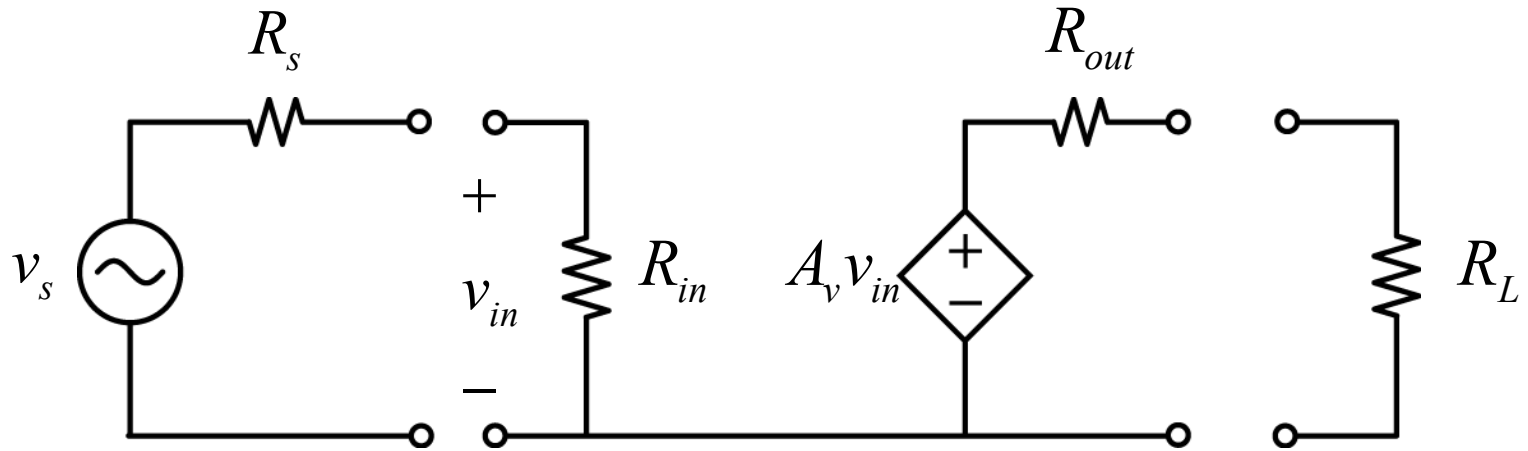


# Small-Signal Two-Port Models

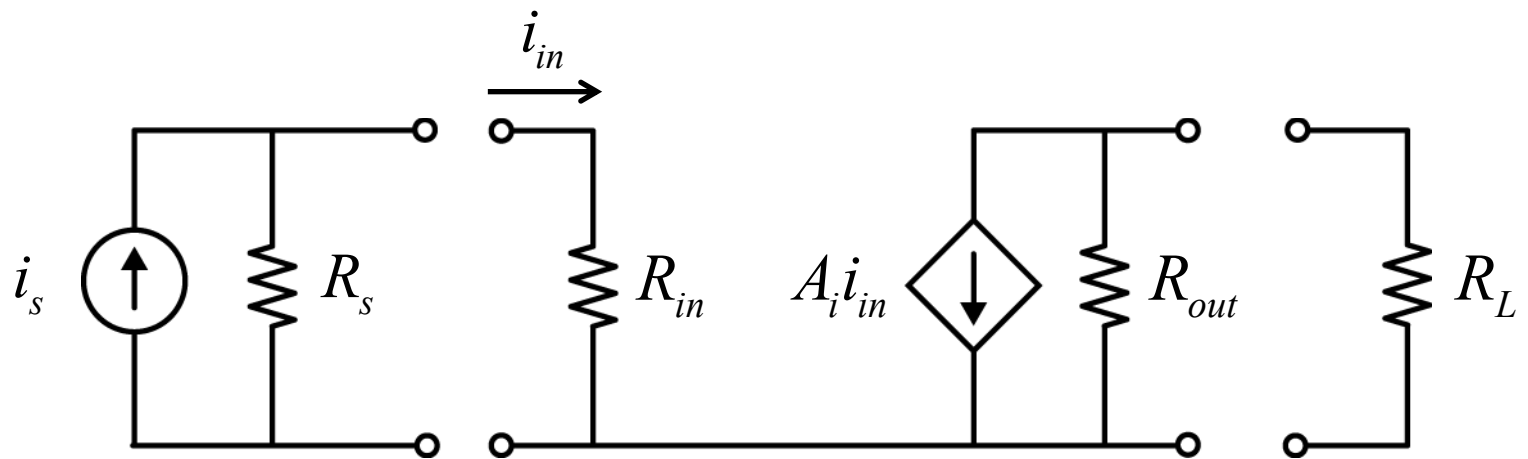


- We assume that input port is linear and that the amplifier is *unilateral*:
  - Output depends on input
  - But input is independent of output.
- Output port: depends linearly on the current and voltage at the input and output ports
- Unilateral assumption is good as long as “overlap” capacitance is small (MOS)

# Two-Port Small-Signal Amplifiers

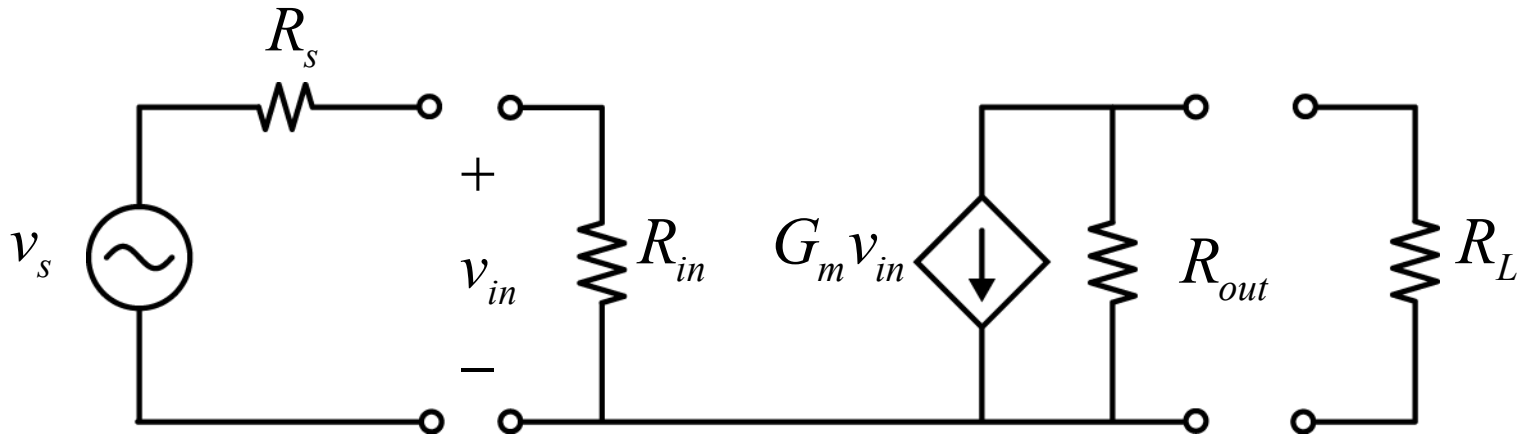


**Voltage Amplifier**

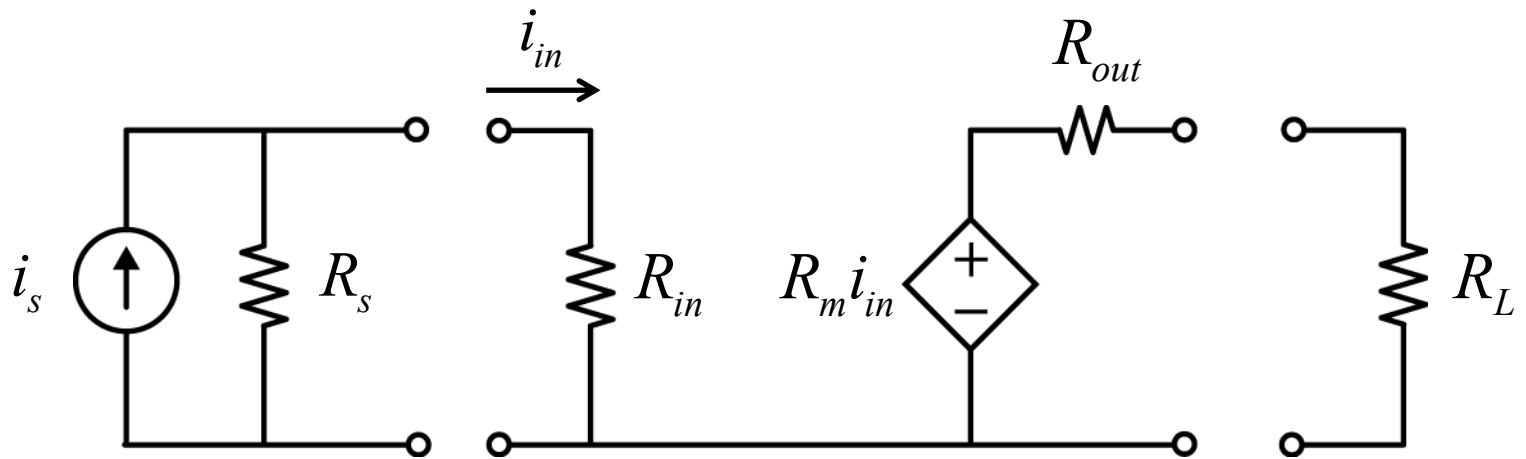


**Current Amplifier**

# Two-Port Small-Signal Amplifiers



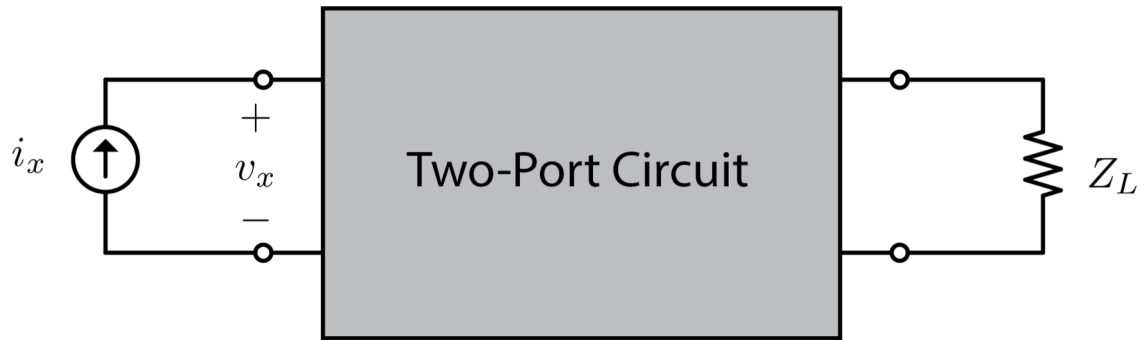
**Transconductance Amplifier**



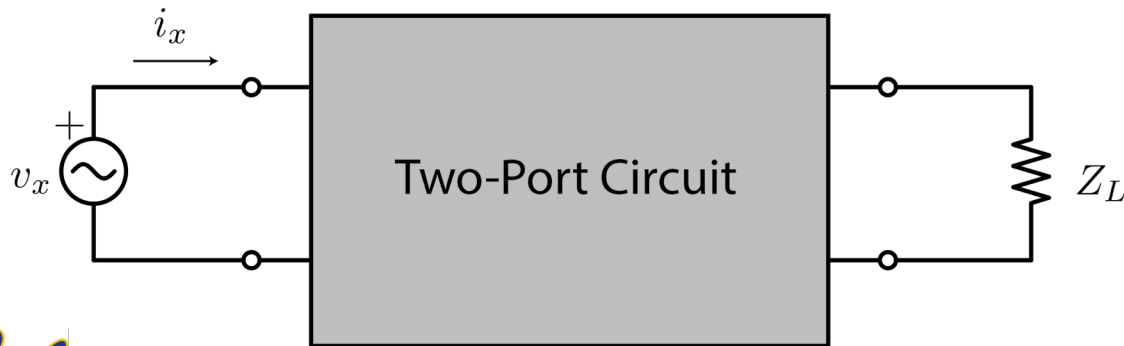
**Transresistance Amplifier**

# Input Impedance $Z_{in}$

- Looks like a Thevenin resistance measurement, but note that the output port has the load resistance attached



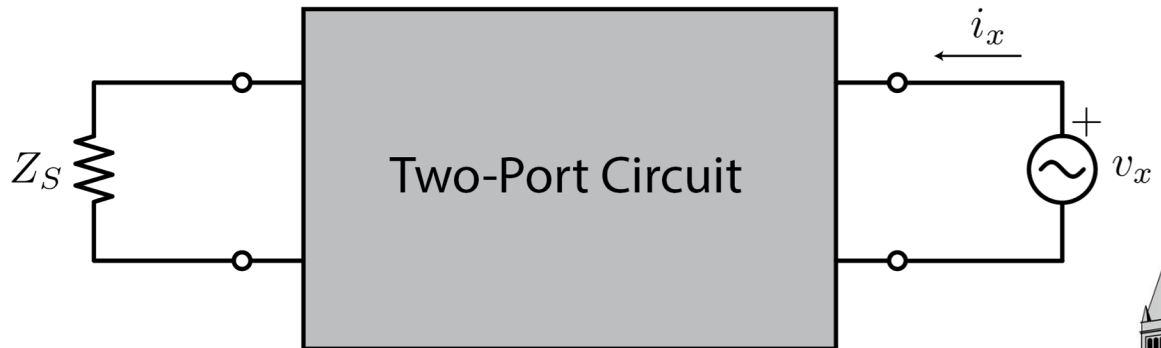
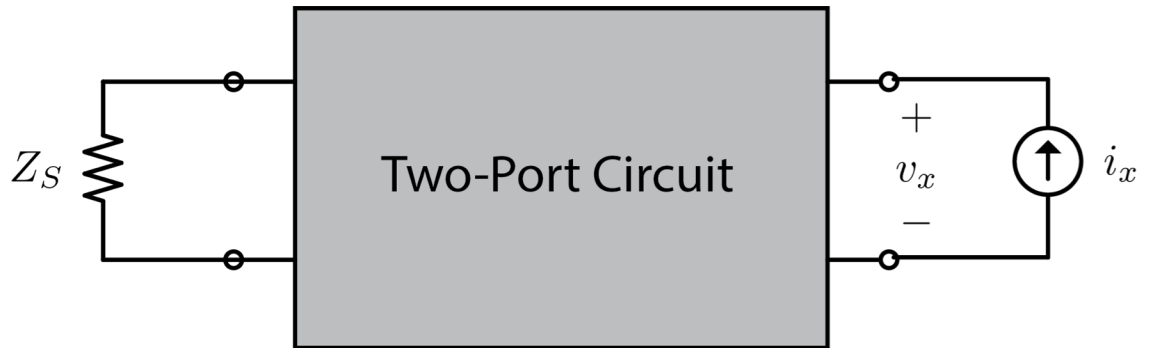
$$Z_{in} = \frac{v_x}{i_x} \left| \begin{array}{l} Z_S \text{ removed,} \\ Z_L \text{ attached} \end{array} \right.$$



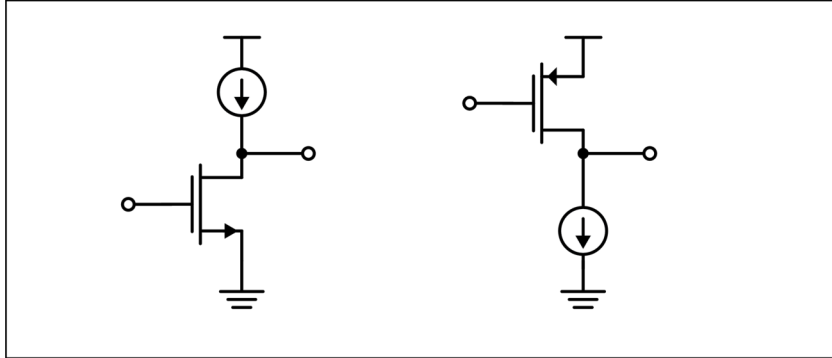
# Output Impedance $Z_{out}$

- Looks like a Thevenin resistance measurement, but note that the input port has the source resistance attached

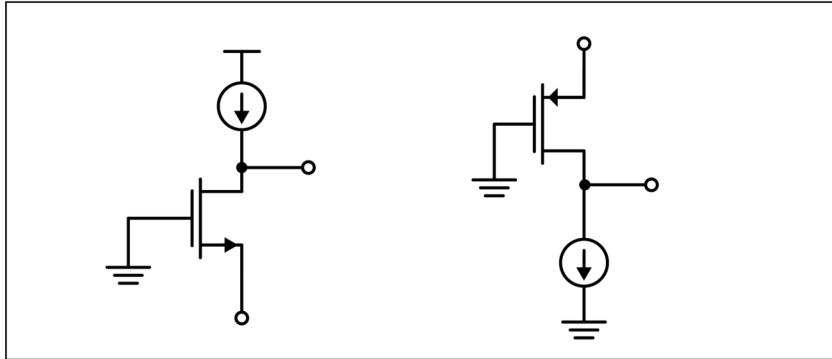
$$Z_{out} = \frac{v_x}{i_x} \left| \begin{array}{l} Z_L \text{ removed,} \\ Z_S \text{ attached} \end{array} \right.$$



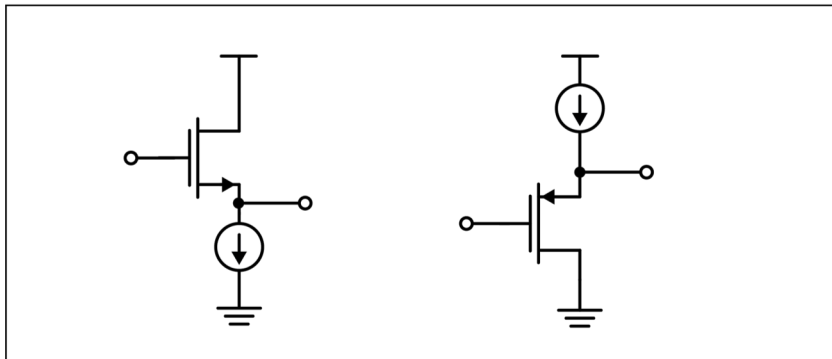
# Single-Stage Amplifier Types



**Common Source (CS)**



**Common Gate (CG)**



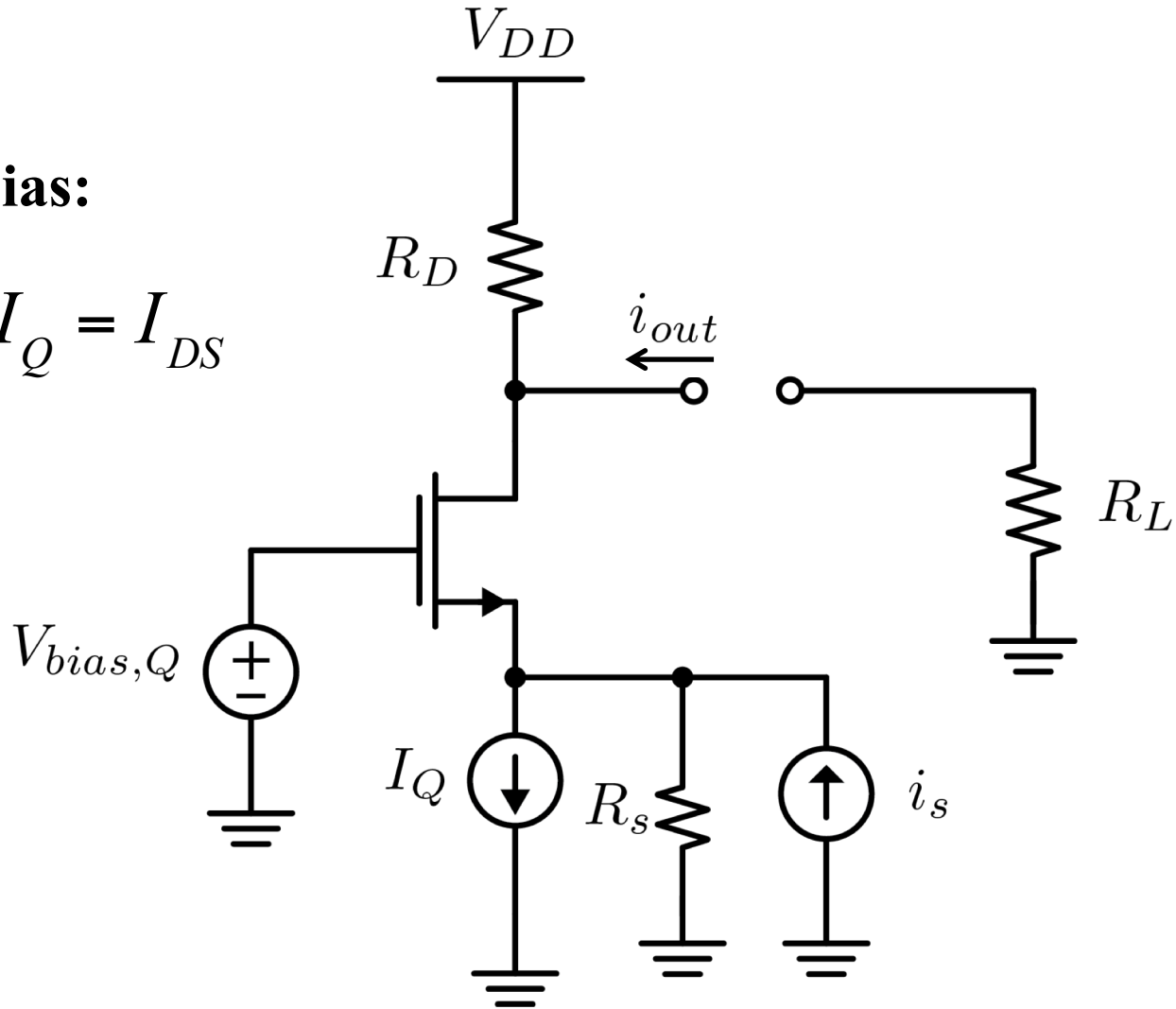
**Common Drain (CD)**



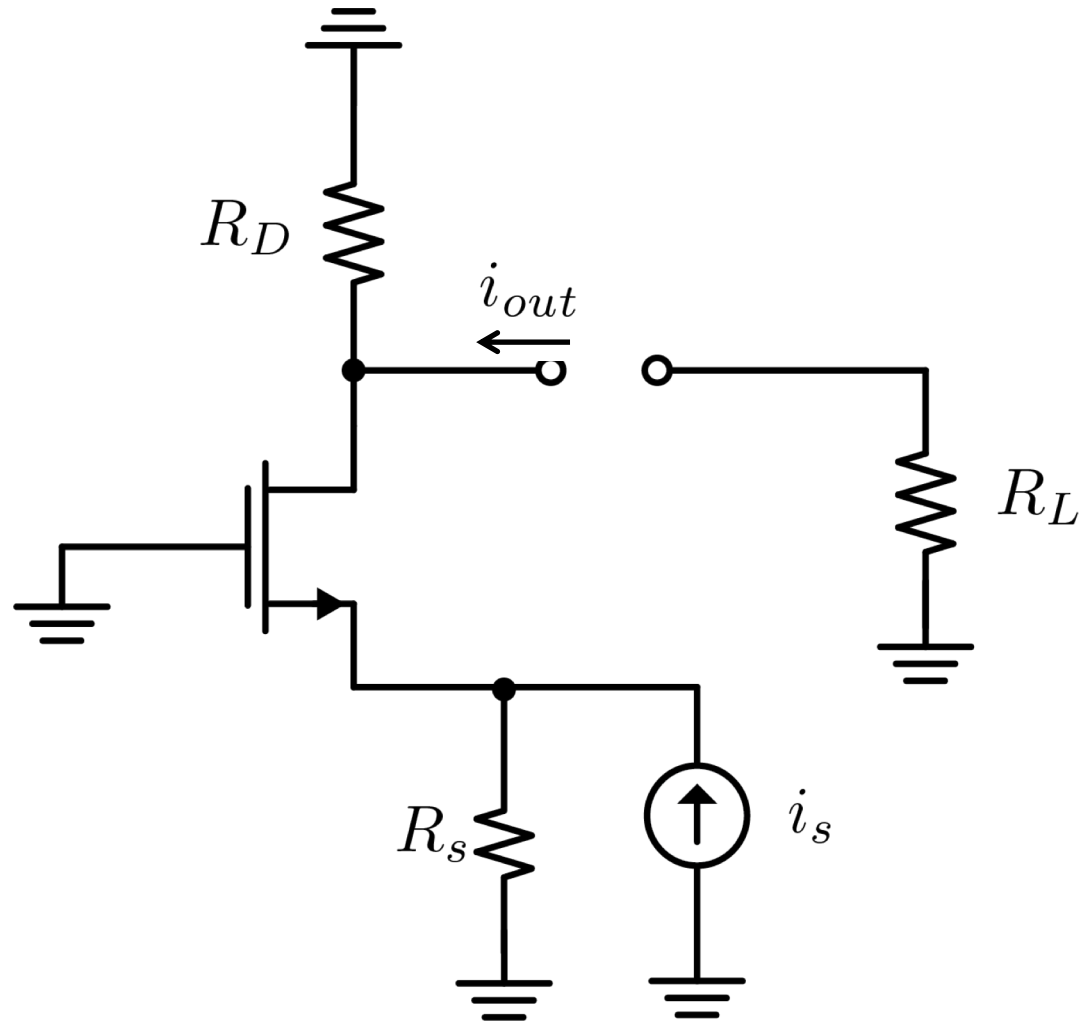
# Common Gate (CG) Amplifier

**DC bias:**

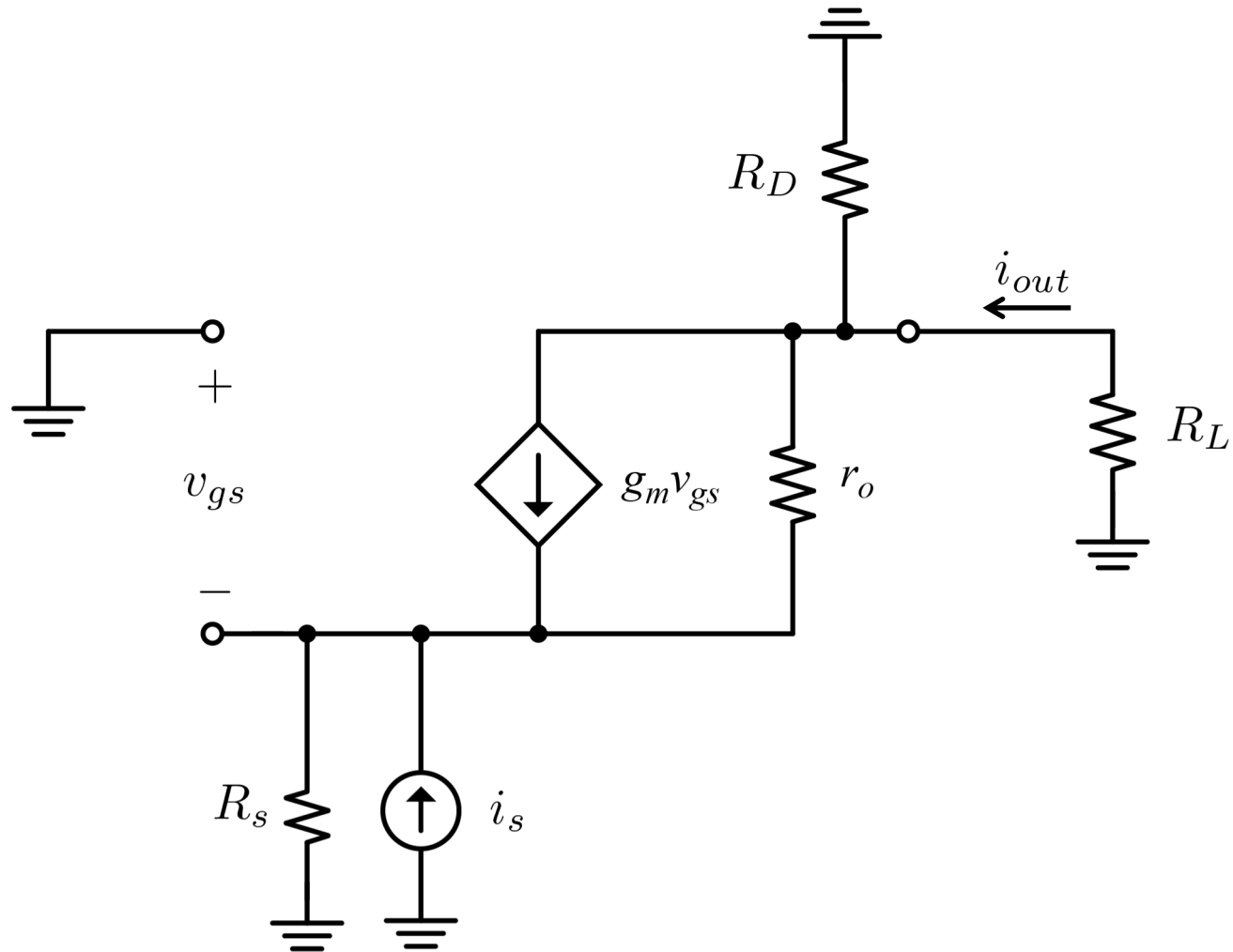
$$I_{SUP} = I_Q = I_{DS}$$



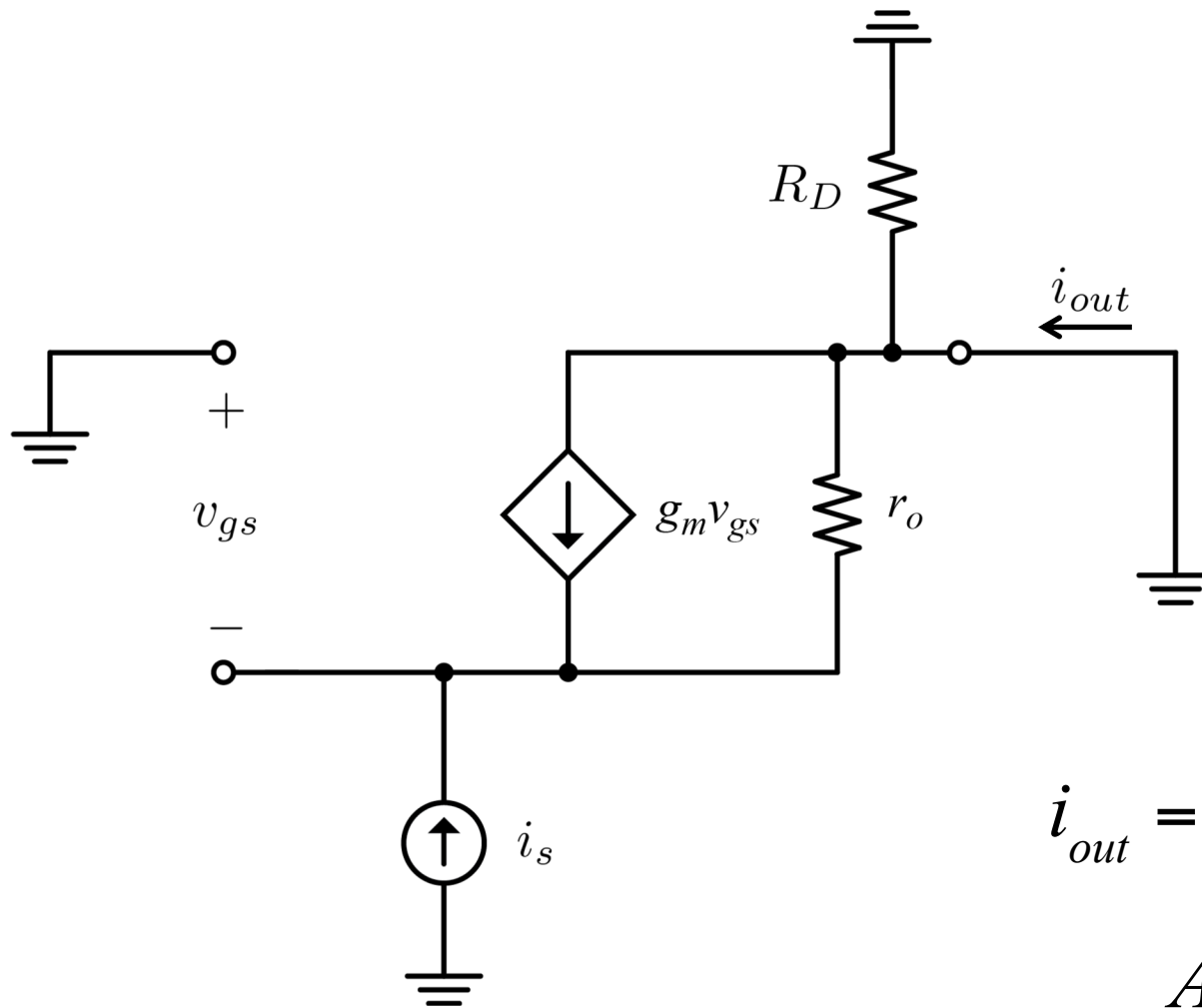
# Common Gate AC Model



# Common Gate Small Signal



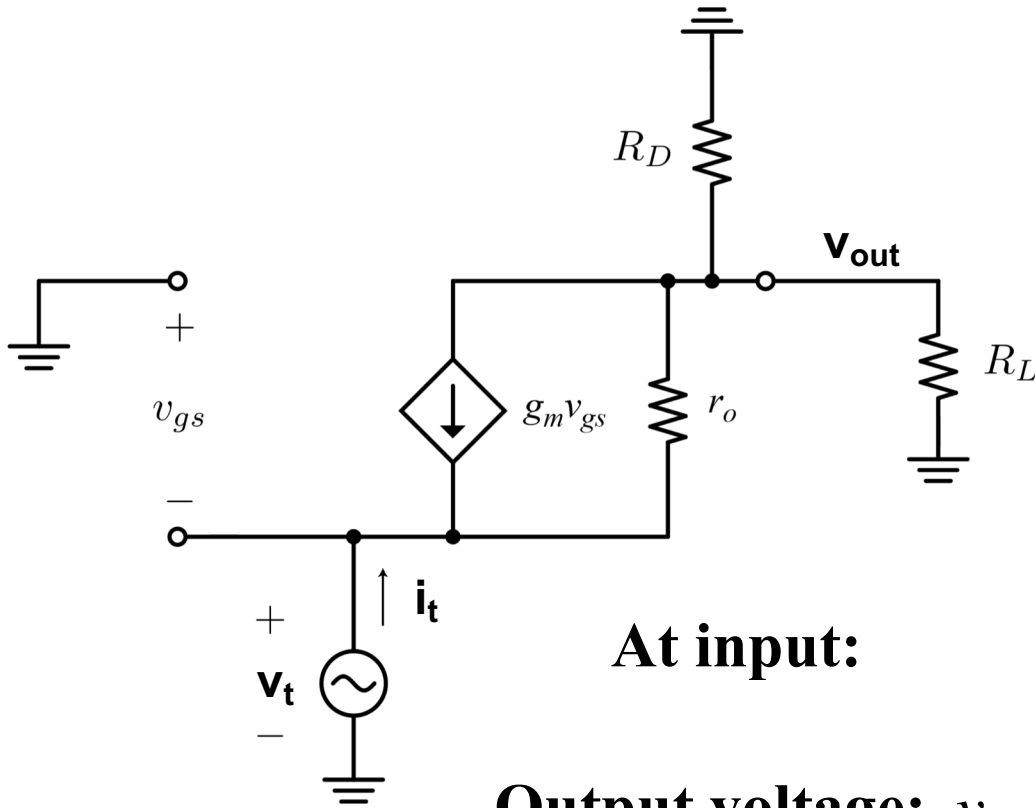
# CG as a Current Amplifier: Find $A_i$



$$i_{out} = i_d = -i_s$$

$$A_i = -1$$

# CG Input Resistance



**At input:**

$$i_t = -g_m v_{gs} + \left( \frac{v_t - v_{out}}{r_o} \right)$$

**Output voltage:**  $v_{out} = -i_d (R_D \parallel R_L) = i_t (R_D \parallel R_L)$

$$i_t = g_m v_t + \left( \frac{v_t - (R_D \parallel R_L) i_t}{r_o} \right)$$

# Approximations...

- We have this messy result

$$\frac{1}{R_{in}} = \frac{i_t}{v_t} = \frac{g_m + \frac{1}{r_o}}{1 + \frac{R_D \parallel R_L}{r_o}}$$

- But we don't need that much precision. Let's start approximating:

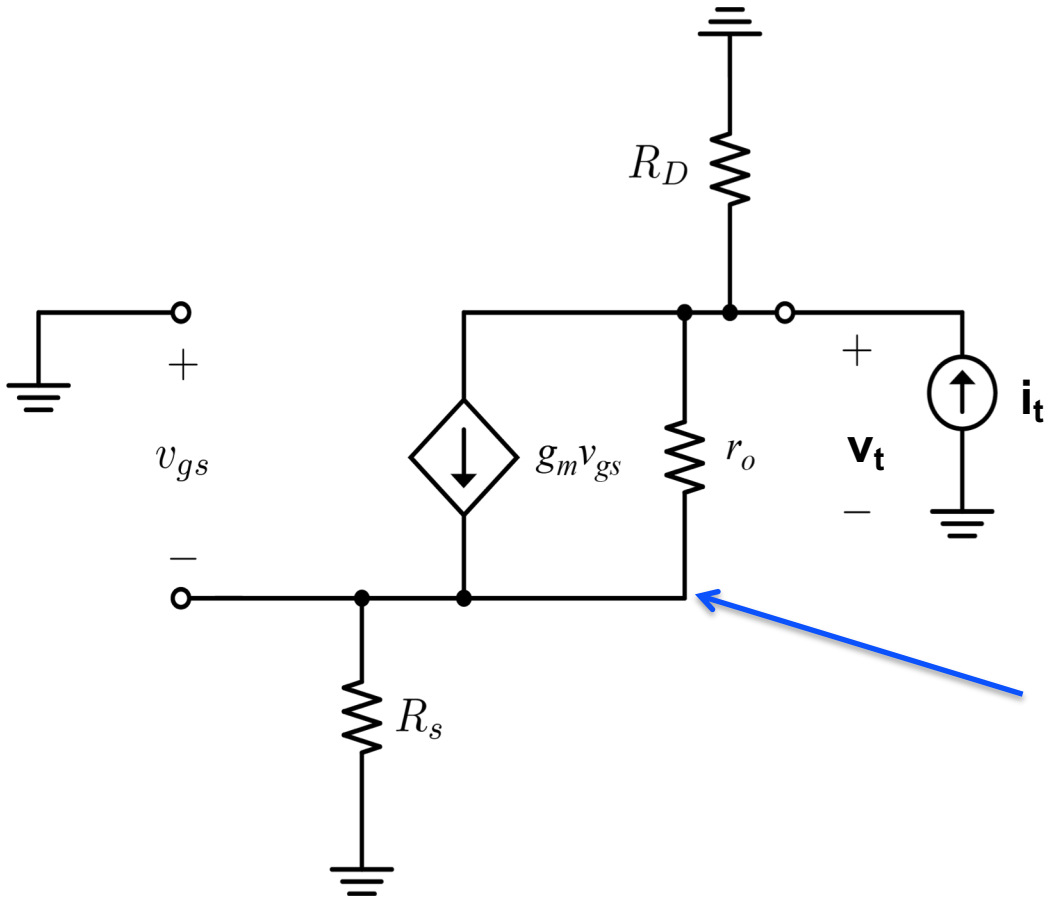
$$g_m \gg \frac{1}{r_o}$$

$$R_D \parallel R_L \approx R_L$$

$$\frac{R_L}{r_o} \approx 0$$

$$R_{in} = \frac{1}{g_m}$$

# CG Output Resistance



$$\frac{v_s}{R_s} - g_m v_{gs} + \frac{v_s - v_t}{r_o} = 0$$

$$v_s \left( \frac{1}{R_s} + g_m + \frac{1}{r_o} \right) = \frac{v_t}{r_o}$$

# CG Output Resistance

Substituting  $v_s = i_t R_S$

$$i_t R_S \left( \frac{1}{R_S} + g_m + \frac{1}{r_o} \right) = \frac{v_t}{r_o}$$

The output resistance is  $(v_t / i_t) || R_D$

$$R_{out} = R_D \parallel \left( R_S \left( \frac{r_o}{R_S} + g_m r_o + 1 \right) \right)$$

$$R_{out} = R_D \parallel \left( r_o + g_m r_o R_S + R_S \right)$$



# Approximating the CG $R_{out}$

The exact result is complicated, so let's try to make it simpler:

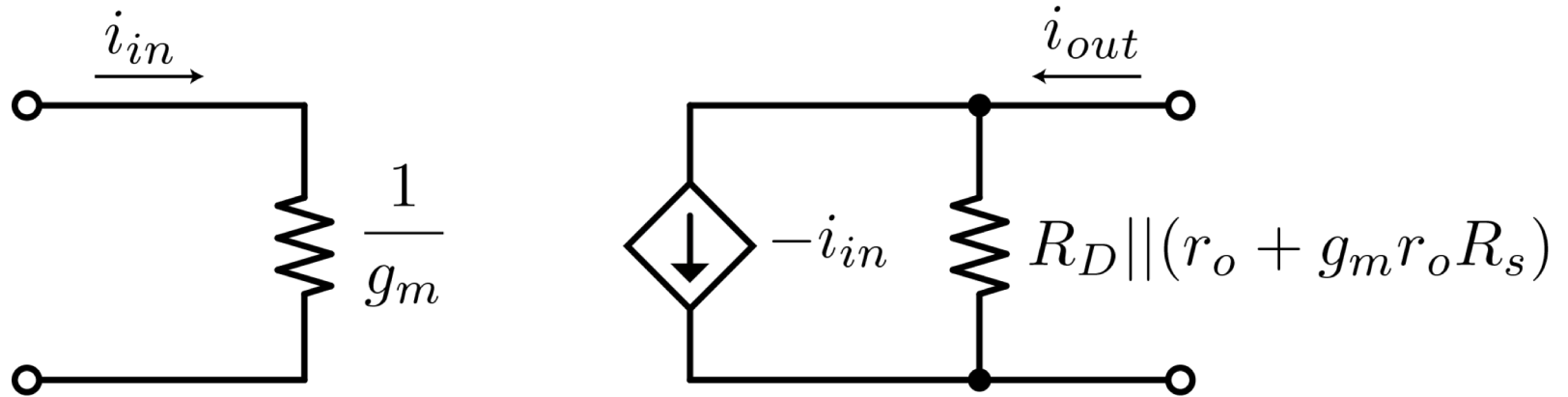
$$g_m \approx 500 \mu S \qquad r_o \approx 200 k\Omega$$

$$R_{out} \cong R_D \parallel [r_o + g_m r_o R_S + R_S]$$

Assuming the source resistance is less than  $r_o$ ,

$$R_{out} \approx R_D \parallel [r_o + g_m r_o R_S] = R_D \parallel [r_o (1 + g_m R_S)]$$

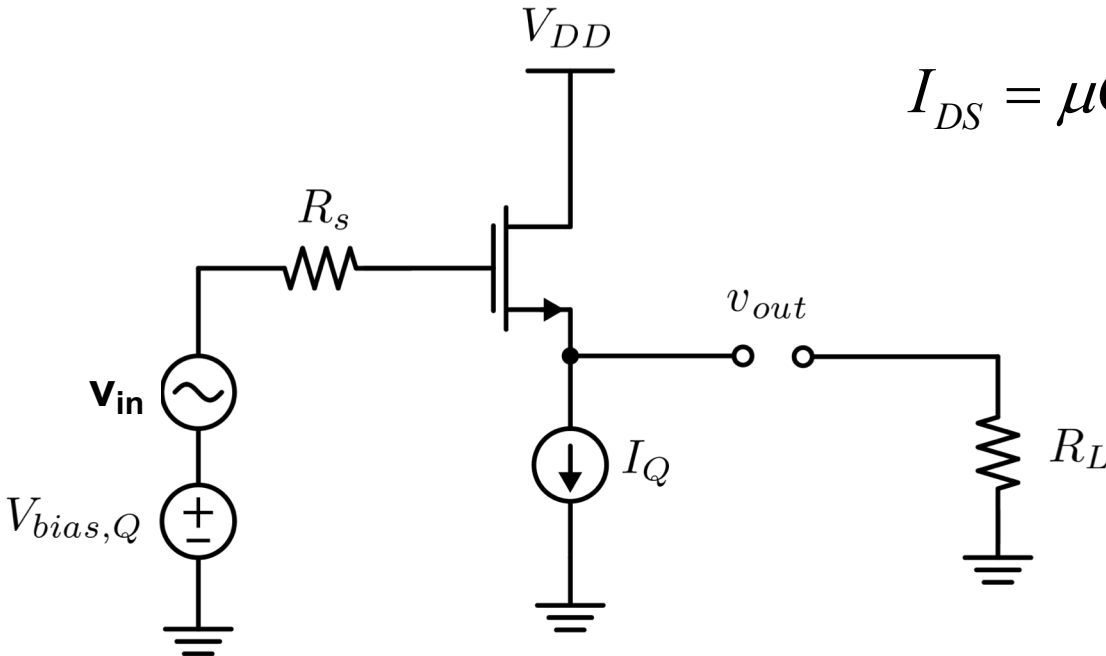
# CG Two-Port Model



- **Function: a current buffer**
  - Low Input Impedance
  - High Output Impedance

# Common Gate as a “V Amplifier”

# Common-Drain Amplifier

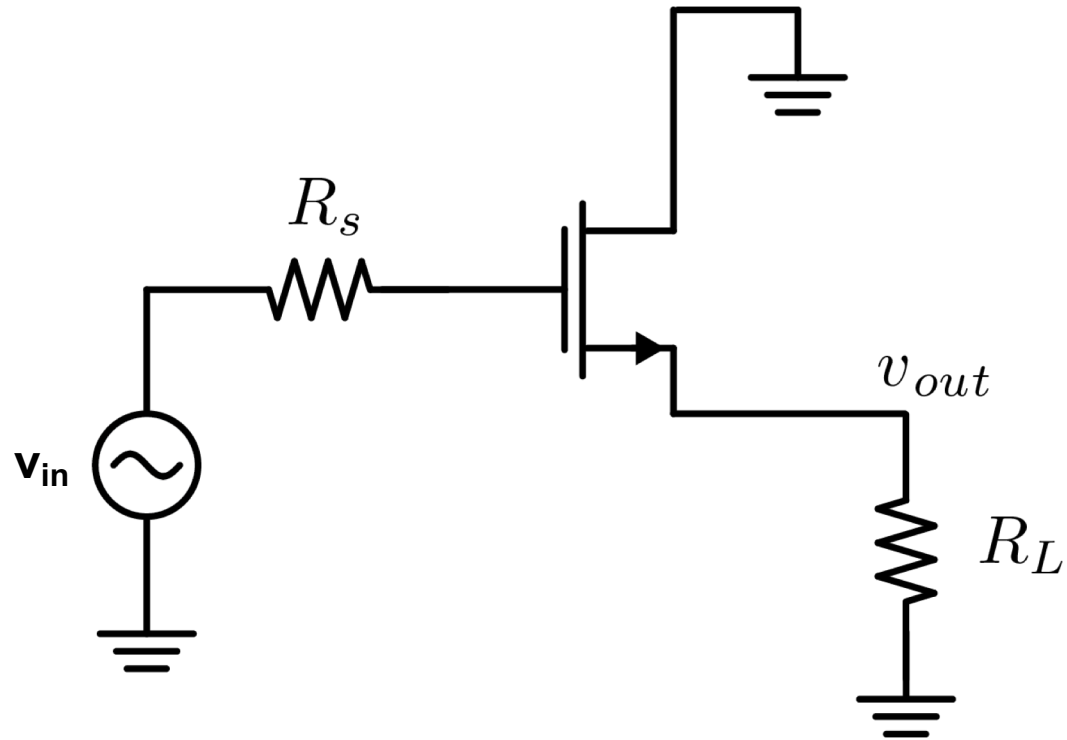


$$I_{DS} = \mu C_{ox} \frac{W}{L} \frac{1}{2} (V_{GS} - V_T)^2$$

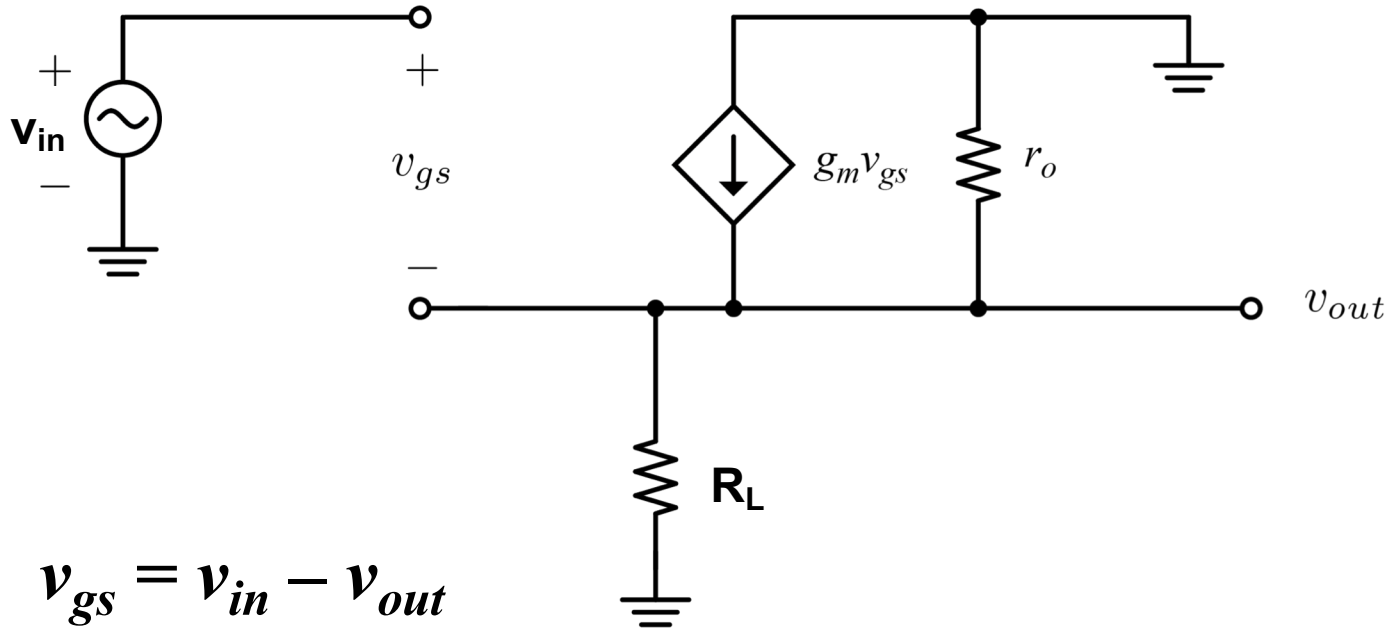
$$V_{GS} = V_T + \sqrt{\frac{2I_{DS}}{\mu C_{ox} \frac{W}{L}}}$$

Weak  $I_{DS}$  dependence

# Common Drain AC Schematic



# CD Voltage Gain



**Note**  $v_{gs} = v_{in} - v_{out}$

$$\frac{v_{out}}{R_L \parallel r_o} = g_m v_{gs}$$

$$\frac{v_{out}}{R_L \parallel r_o} = g_m (v_{in} - v_{out})$$

# CD Voltage Gain (Cont.)

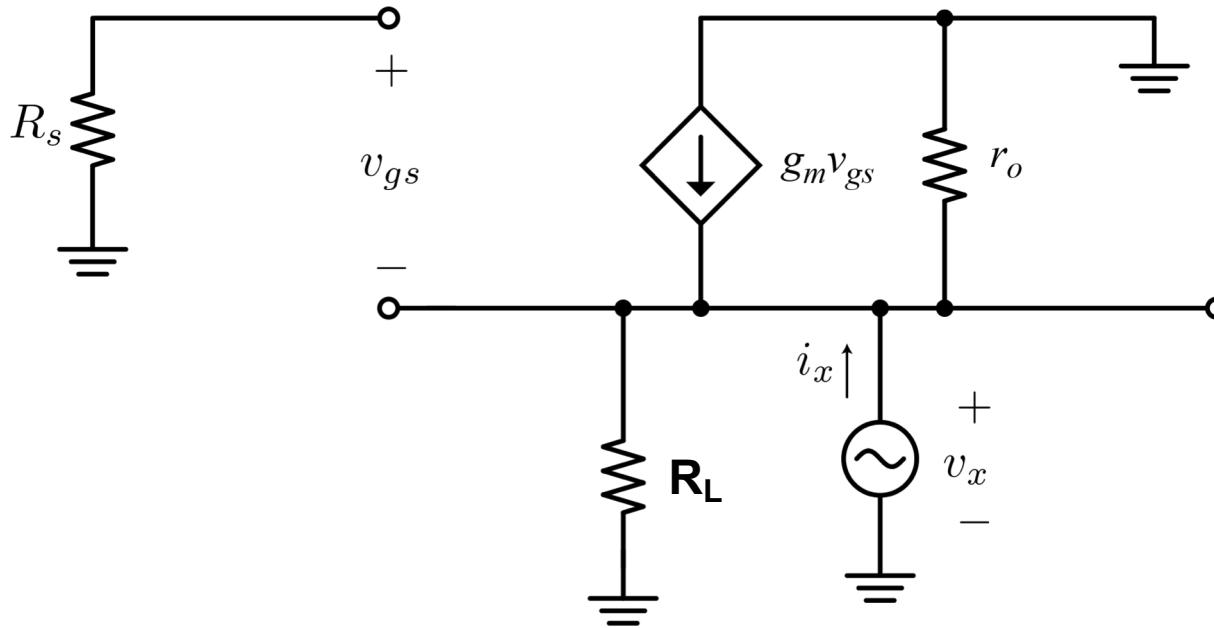
**KCL at source node:**

$$\frac{v_{out}}{R_L \parallel r_o} = g_m (v_{in} - v_{out})$$
$$\left( \frac{1}{R_L \parallel r_o} + g_m \right) v_{out} = g_m v_{in}$$

**Voltage gain:**

$$\frac{v_{out}}{v_{in}} = \frac{g_m}{\frac{1}{R_L \parallel r_o} + g_m}$$
$$\frac{v_{out}}{v_{in}} \approx \frac{g_m}{1/R_L + g_m} \approx 1$$

# CD Output Resistance



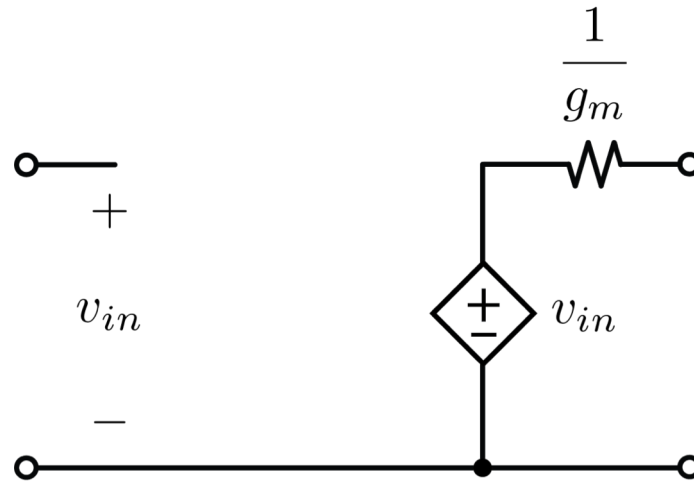
**Sum currents at output (source) node:**

$$i_x = g_m v_x \quad R_{out} = r_o \parallel R_L \parallel \frac{v_x}{i_x} \quad R_{out} \approx \frac{1}{g_m}$$



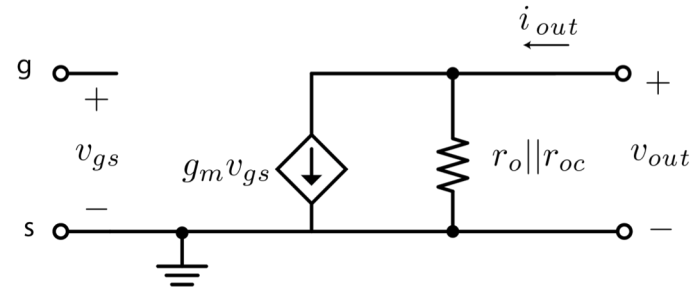
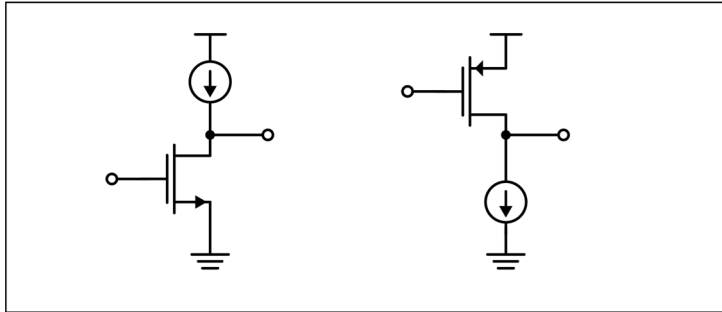
# CD Output Resistance (Cont.)

$$r_o || R_L \ll \frac{1}{g_m} \Rightarrow \text{Ignore } r_o || R_L$$

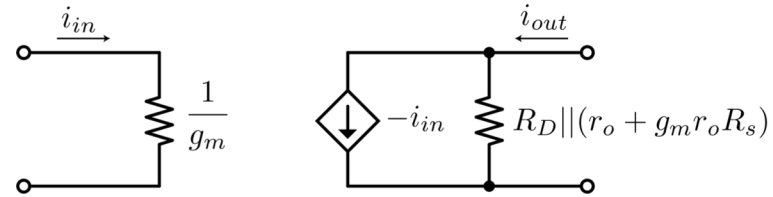
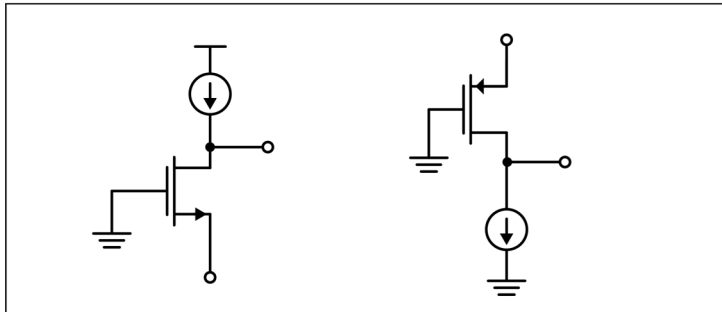


- **Function: a voltage buffer**
  - High Input Impedance
  - Low Output Impedance

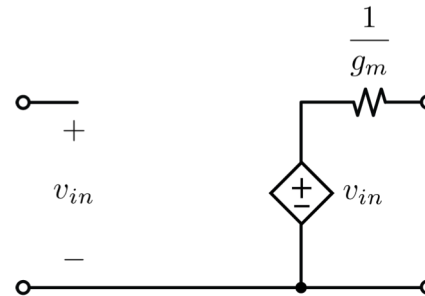
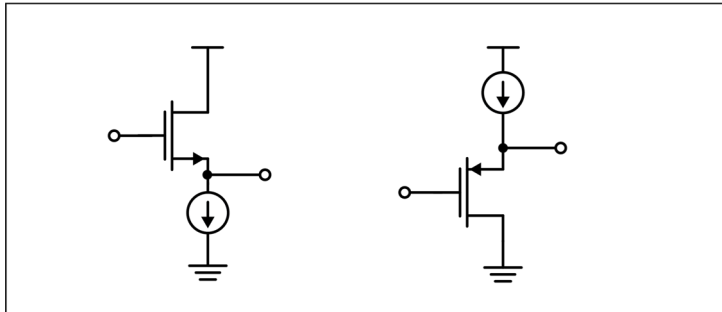
# Transistor Amplifiers → Gm/V/I



**Gm Amplifier  
Common  
Source**



**I-Buffer  
Common  
Gate**



**V-Buffer  
Source  
Follower**